
Testing instrument capabilities from simulations

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OVERVIEW

Testing instrument capabilities from **simulations**

- **Simulation of the Instrument**

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Testing **instrument** capabilities from **simulations**

- **Simulation of the Instrument**
- **Simulated Instrument vs. Real Instrument**

OVERVIEW

Testing instrument capabilities from simulations

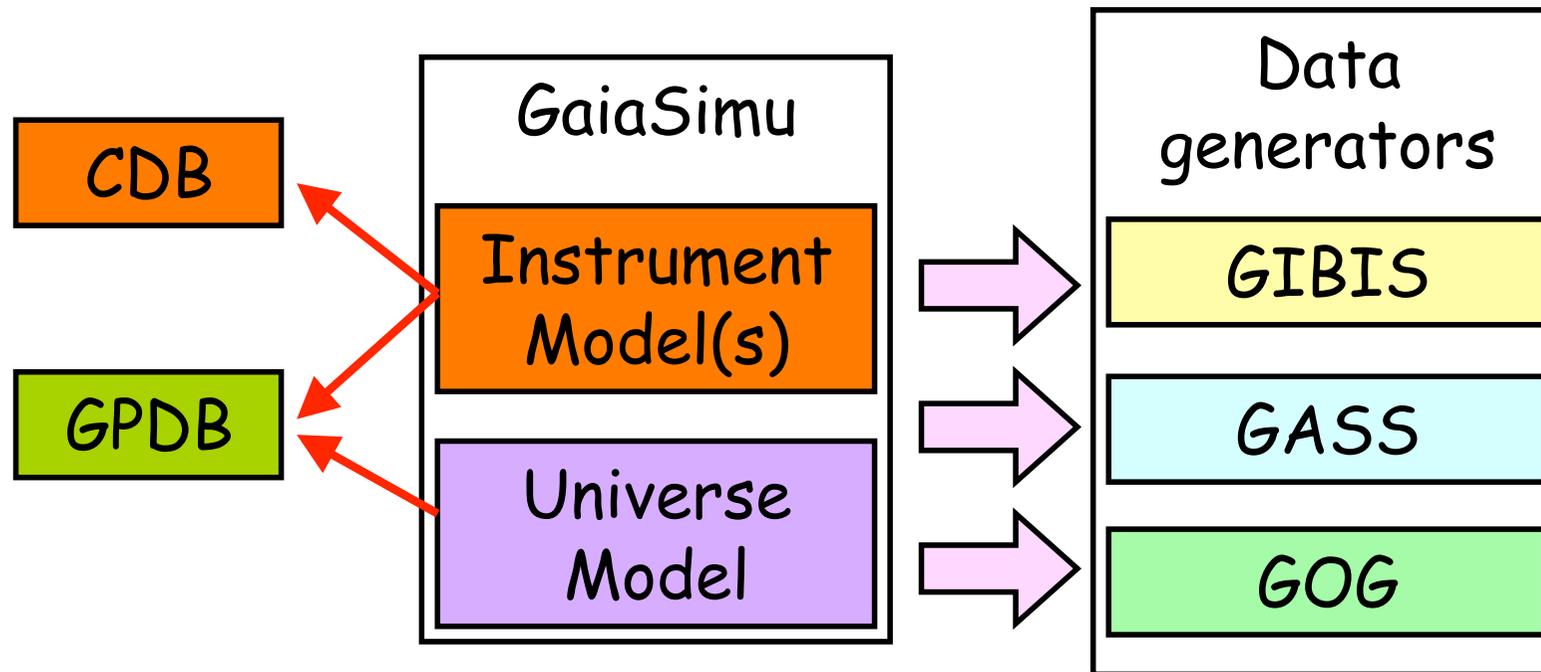
- Simulation of the Instrument
- Simulated Instrument vs. Real Instrument
- Methods for testing capabilities

OVERVIEW

Testing instrument capabilities from simulations

- Simulation of the Instrument
- Simulated Instrument vs. Real Instrument
- Methods for testing capabilities
- example: astrometry

Instrument simulation in CU2 - overview



Data generators characteristics vs. Instrument model

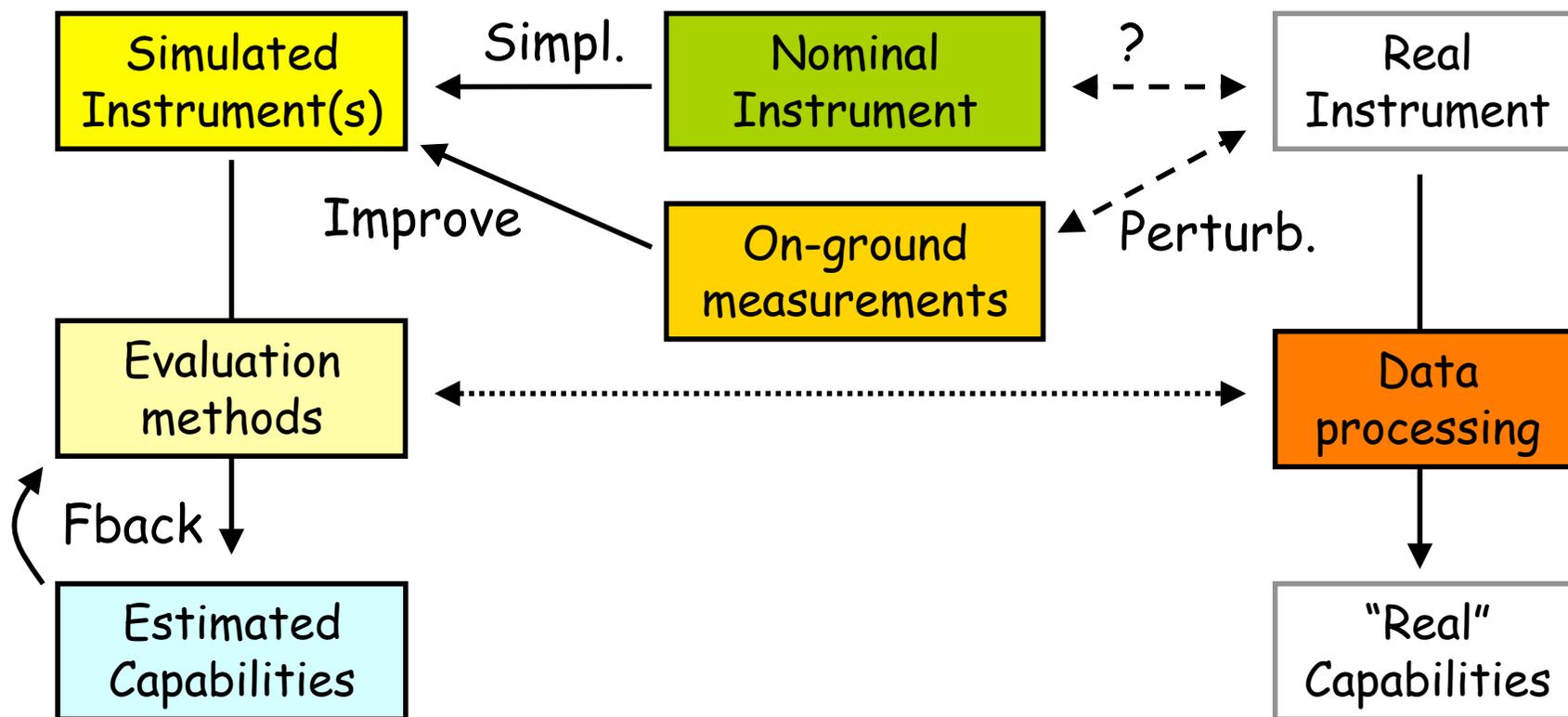
- *GIBIS*: simulation of data at pixel level. As realistic as possible for limited regions of the sky and over short periods of time.
- *GASS*: simulation of telemetry stream. Use simplified models of the instrument. Large amount of data over a significant part of the planned Gaia mission duration
- *GOG*: simulation of observed object lists + intermediate/end of mission Gaia data for given source. Use error models.

-> Need different models of the same subsystems/effects
(problems: duplication and consistency)

Simulated vs. Real Instrument

- instrument is not completely built yet
- many subsystems already tested or being tested now
- In any case, knowledge of the real instrument can/will be only partial:
 - Many relevant instrument parameters not measured (or non-measurable) on-ground
 - In-flight configuration and environmental conditions different from nominal / predicted ones.

Simulated vs. Real Instrument

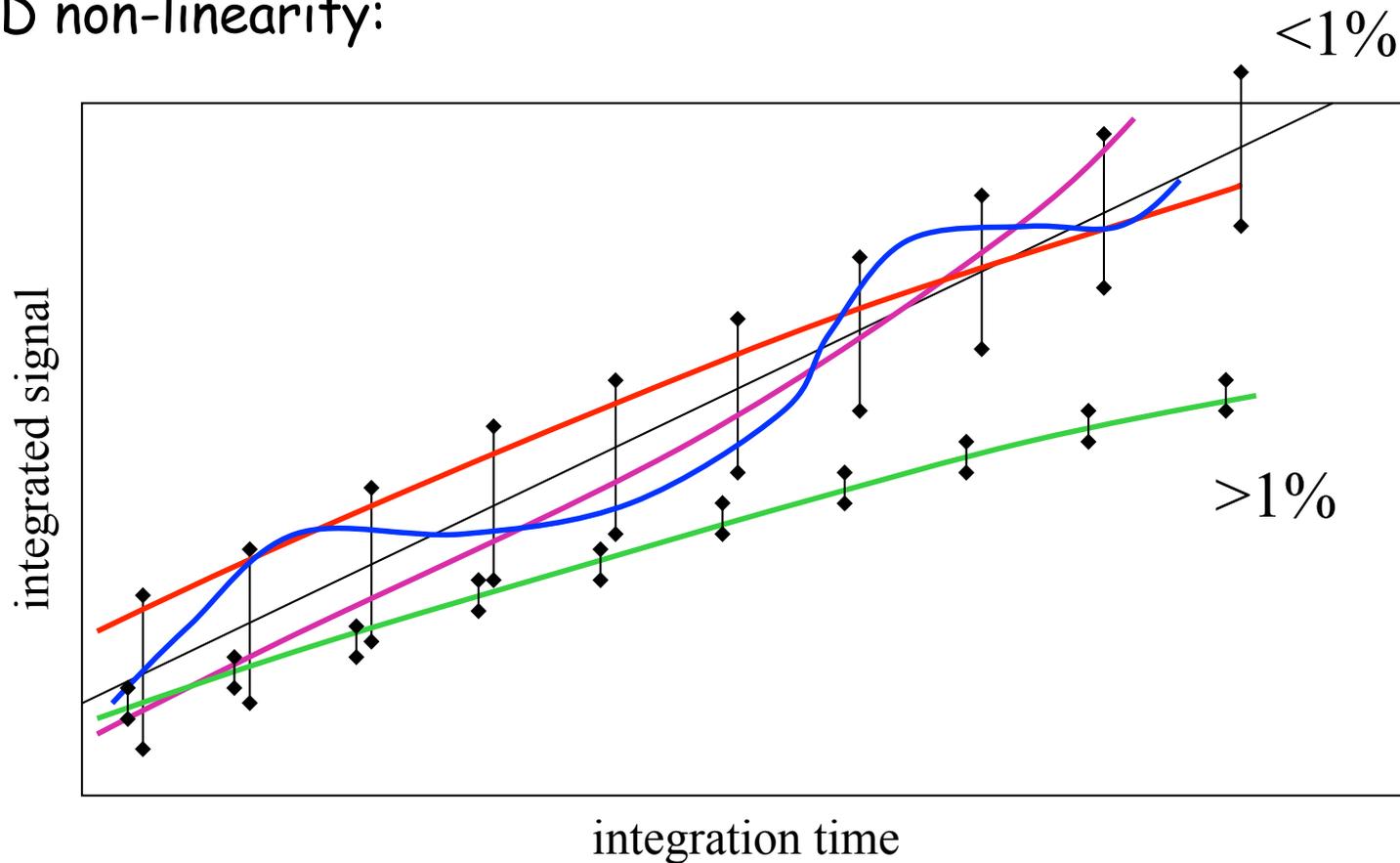


Further note on on-ground measurements

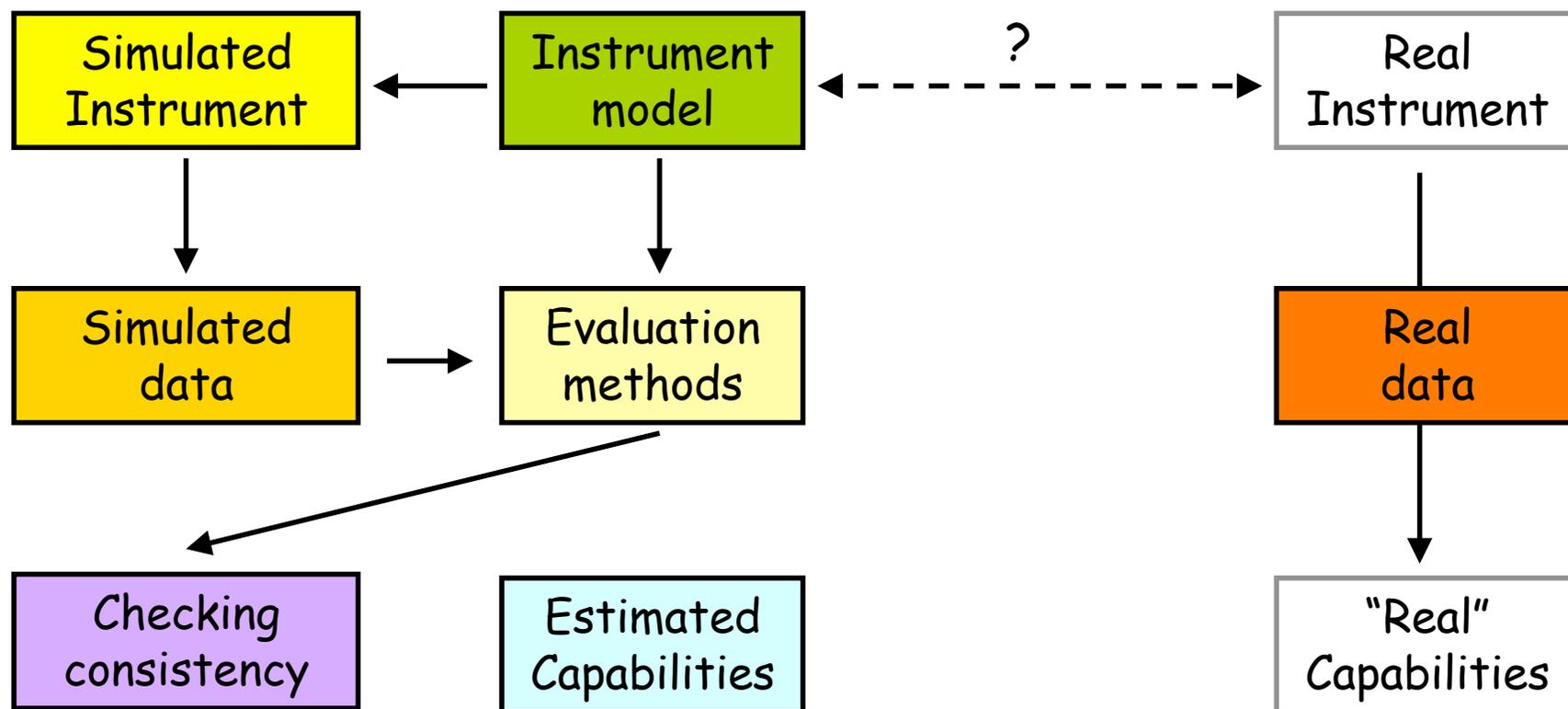
- Usually made by industry to convince ESA that requirements are fulfilled
- Requirement fulfilled doesn't mean "proper" knowledge of the instrument
- Example: CCD non-linearity
- Req may sound like "CCD non-linearity calculated in some way shall not exceed 1%"
- For calibration purposes, you may prefer a non-linearity $> 1\%$, but a well known non-linearity profile vs. integration time

Further note on on-ground measurements

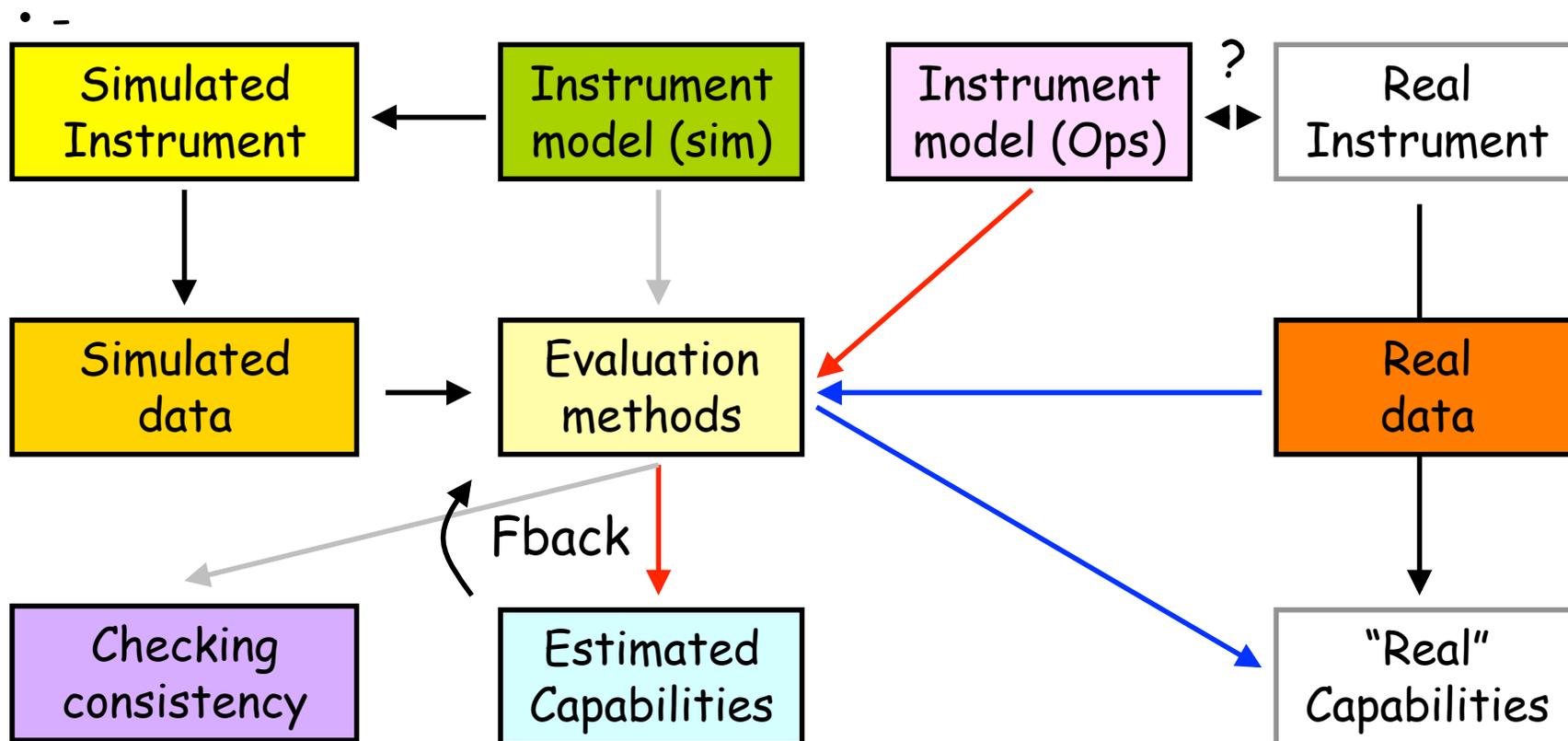
CCD non-linearity:



Evaluation methods



Evaluation methods



Example: astrometric performance

PSF/LSF model for simulations

The model is based on a dual representation:

- **numerical library for GIBIS**. The starting point is a numerical library where the elements are generated from the optical design of the instrument (CodeV generated WFEs, 1 per CCD) plus some ad-hoc effects (TDI, pixel, etc).
- **analytical library for GASS/GOG**. The elements of the library are generated from bi-quartic B-spline fittings of the numerical library. Interpolation for any point in the coefficients grid available.
- Both the analytical and the numerical representations provide the integrated flux over one pixel, normalised to the total integrated flux

Note that:

- many effects can be introduced at the level of the numerical library and they will automatically be present in the analytical representation with no need to develop specific models for *GASS/GOG*
- the analytical representation requires a minimised number of computations in *GASS/GOG*
- nonetheless, many effects are not usefully described by means of precomputed libraries (CTI, noise, magnitude, non-linearity/saturation, ...) and are treated separately

PSF Numerical (discrete sampling) Library

Generated as follows (starting from nominal WFEs, PS-010):

- monochromatic PSFs (250-1050 nm) with steps of 1 nm
- 11 quasi-monochromatic PSF (using triangular bands, LL-080)
- pixel, TDI, attitude errors, optical distortion, charge diffusion (effqmPSF)
- source motion and gates are treated separately
- Polychromatic PSF can be computed by linear combination of effqmPSF + source spectrum
- Polychromatic PSF library for colour index V-I also available.

Analytical library

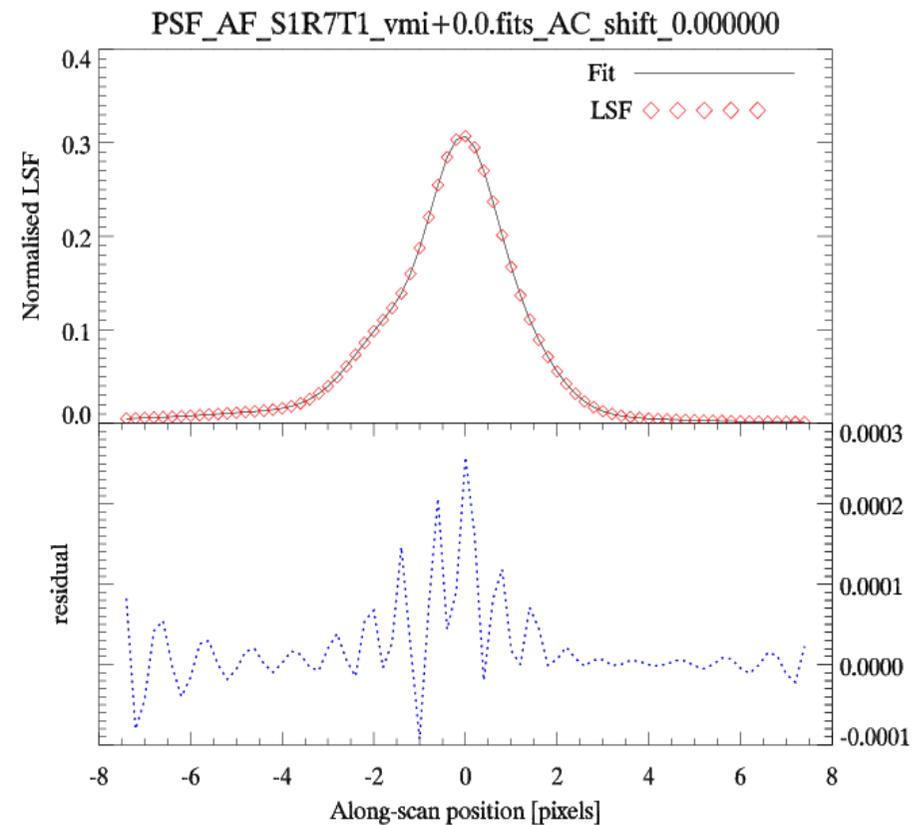
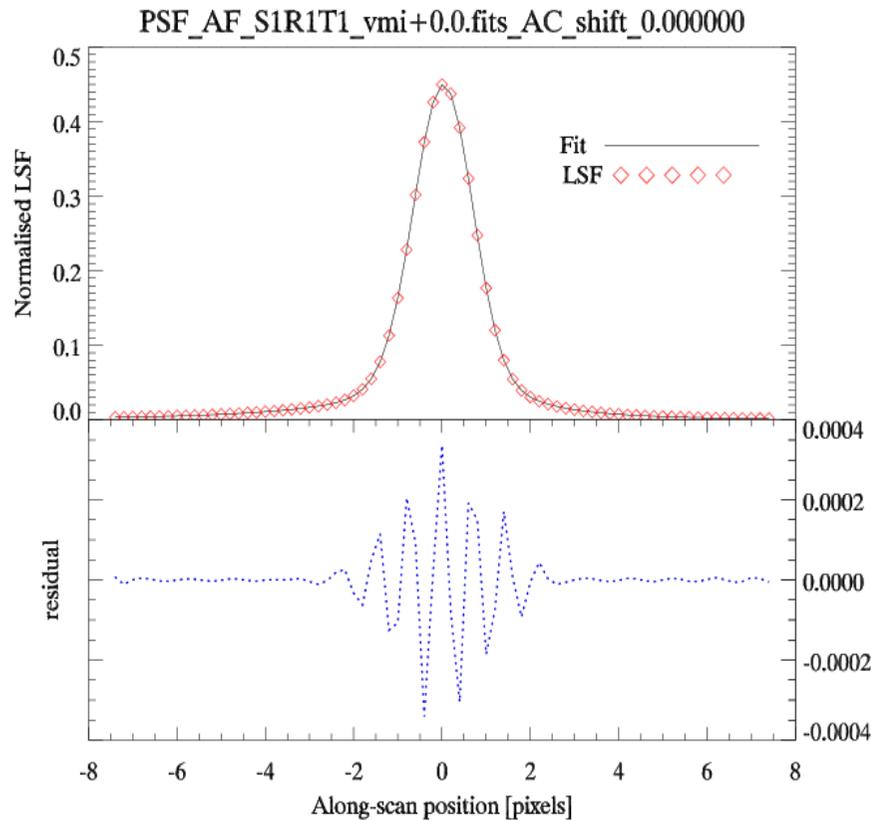
Analytical library:

- Fitting functs: Bi-quartic B-Spline + wings (LL-066). Result: Analytical function giving pixel readout for any (continuous) AL position (33 params)
- Details of the analytical library coeffs calculation in DB-009
- Interpolation in coefficients space domain (DG-014)

Parameter	SM	AF	
Telescopes	2	2	<- Size of Parameter space domain
FoVs	7	62	
Triang. bands (wavelength)	11	11	
(V-I)	12	12	
	154	1364	

Analytical model - AF (example)

• S1R1T1 vs. S1R7T1 ($V-I = 0.0$)



Other talks related to instrument modeling

- F. van Leeuwen - Modeling the attitude: lessons learnt from Hipparcos
- D. Riquez - Modeling the attitude of the Gaia Satellite
- M. Weiler - Implementation of CTI models in GIBIS
- T. Prod'homme - Radiation effects on Gaia CCDs

LSF - Signal profile modeling

- Problem treated in LL-084, MG-009
- The LSF model can be written as a linear combination of basis functions

$$\tilde{L}(u) = \sum_{m=0}^N c_m B_m(u)$$

- How many parameters N do we need to properly model the signal profile?
- Which are the basis functions that provides the most accurate approximation of the LSF?
- How good this approximation is (as a function of N)?

LSF - Signal profile modeling

Principal Component Analysis provide a solution to this problem (LL-084)

- The model of the signal profile is obtained starting from a large sample of LSFs, generated with many different WFEs and SEDs over M points
- Any LSF can be written as linear combination of basis vectors

$$\vec{L} = c_0 \vec{B}_0 + \sum_{m=1}^M c_m \vec{B}_m$$

where B_0 is the mean LSF and B_m are obtained from the covariance matrix (deviations wrt the mean profile)

The truncated expansion $LSF' = c_0 B_0 + \sum_{m=1}^{N < M} c_m B_m$ has minimum expected RMS error among all linear models with N free parameters (under proper hypothesis)

LSF - Signal profile modeling

Another approach is also proposed (MG-009):

signals are expected to be reasonably close to the ideal case ->
they fit a context of small perturbations/aberrations

- ideal instrument ->

$$F_0(u; \lambda) = \left(\frac{\sin \rho}{\rho} \right)^2, \quad \rho = \frac{\pi D}{\lambda f} u$$

- perturbations ->

$$F_n(u; \lambda) = \frac{d}{du} F_{n-1}(u; \lambda) = \frac{d^n}{du^n} F_0(u; \lambda)$$

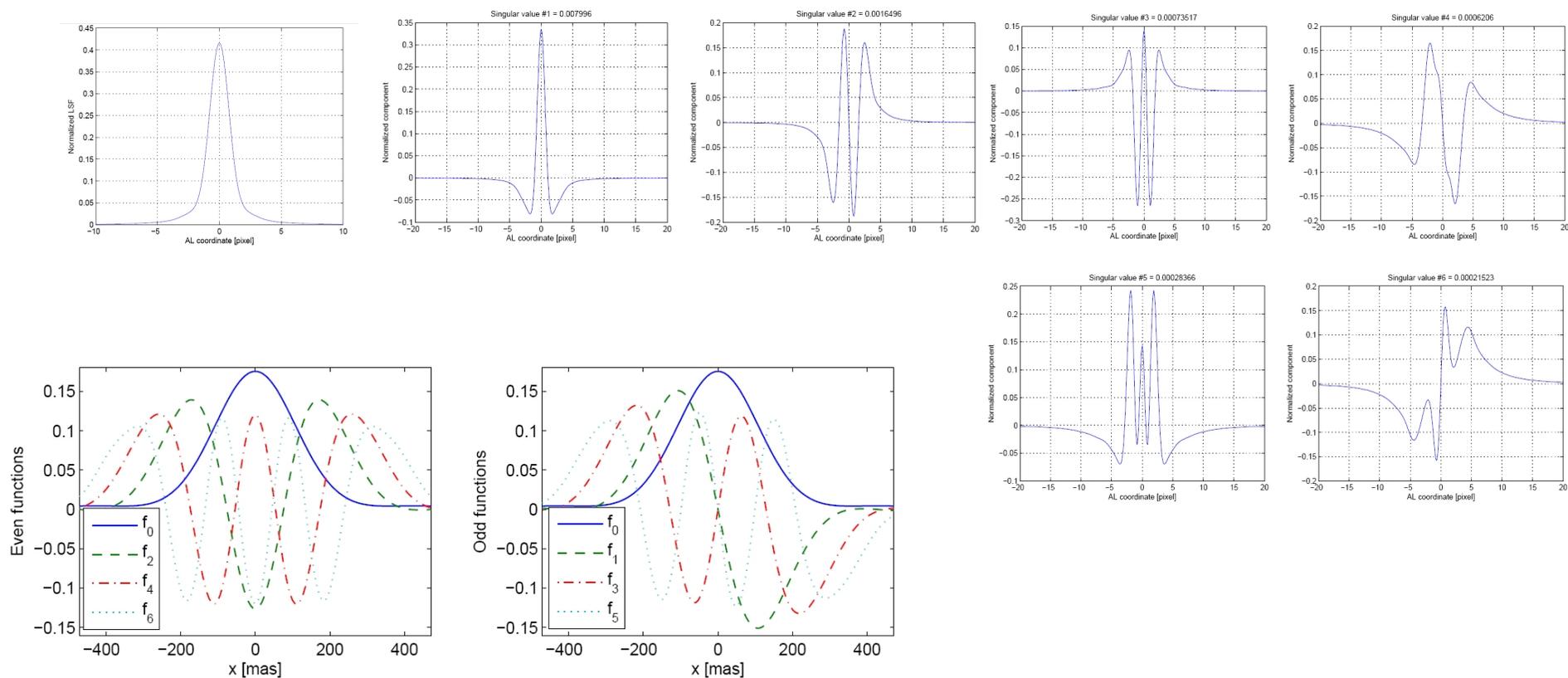
- polychromatic LSF ->

$$F_0(u) = \int S(\lambda) F_0(u; \lambda) d\lambda$$

- ortho-normalisation ->

$$\sum_k F_p(u_k) F_q(u_k) = \delta_{pq}$$

LSF - basis functions

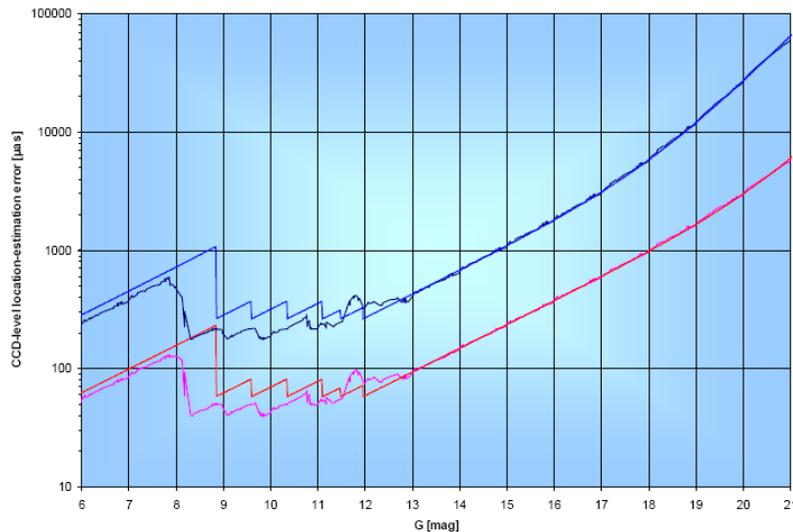


Signal profile modeling - summary

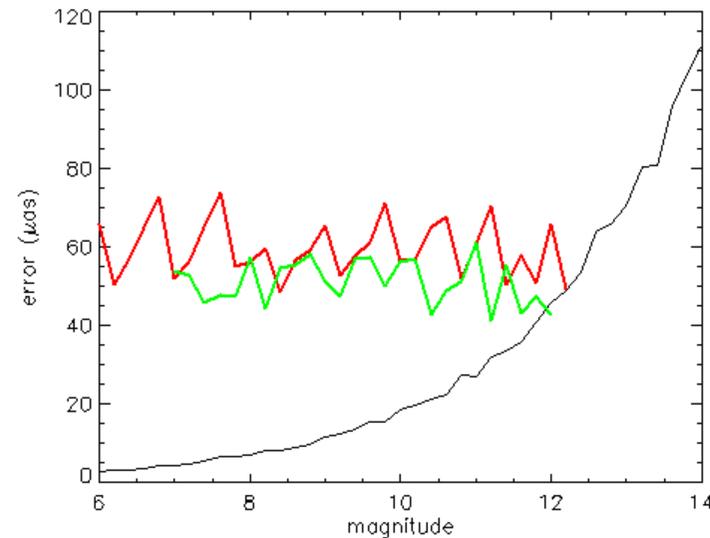
LL-084	Model	MG-009
~ 10 - 11	Number of params	~ 10 - 11
PCA (mean LSF + cov. + interpolation)	Basis functions	$(\sin x/x)^2$ + derivatives
10^{-3}	RMS residual (5 pars)	
10^{-4}	RMS residual (10 pars)	10^{-4}
	astrom. residual (μ ,rms)	(7 μ as ; < 1 μ as)
Tukey's biweight (LL-068)	Localisation process	COG
simulated + real (camp. #3)	Data	simulated

Astrometric accuracy

- First tests with this models (Analytical LSF + PCA) in IDT 8.0
- Other independent astrometric accuracy analysis:
- *GAAT* (JDB-053, JDB-055)



Bright Stars (DG-001, ML-025)



- Similar results in the magnitude range [6,14]

Summary

- Simulation of the instrument must take into account all major effects
- Effects introduced with rather simple models may already provide a satisfactory first order description
- Further refinements using more complex/sophisticated models fight with:
 - "distance" between the nominal and the real instrument
 - Computing time, data storage, et cetera
- Requirements satisfied does not mean you are able to properly model/simulate your instrument
- Tests of instrument capabilities using simulations are reliable only up to a certain level (they provide anyway a first approximation of what you can expect)
- Gaia astrometric performances will probably be limited by poor knowledge of the real signal profile

Thank you